

# LPG BASIC PRINCIPLES AND PRACTICES

One\ LPG physical and chemical properties

Two \ LPG System components

LP gas Tanks

- Codes of Design & Manufacturing , ASME versus EN

Regulators

- 1st Stage & 2nd Stage regulators.

Vaporizers

- Direct Fire
- Electrical

Safety Equipment

### Three \ Design Elements of LP-Gas System

Introduction to the international standards and codes regarding the use of gas. (NFPA 58 \ NFPA 54 \ Gas Transmission pipe lines) in term of:

- Container Locations & preparations.
- Cylinder & Tank Manifolding
- Pipe Selection
- Pipe Sizing
- Regulator selection
- 2 Stage Regulation
- Safety Precautions and measures including safety equipment and accessories.( anti seismic valves, excess flow, fused, solenoid valves, gas leakage detectors, change over panels, gas meters, relief valves)
- Testing methods

Four \ Natural Gas Vs. LPG , applications and characteristics

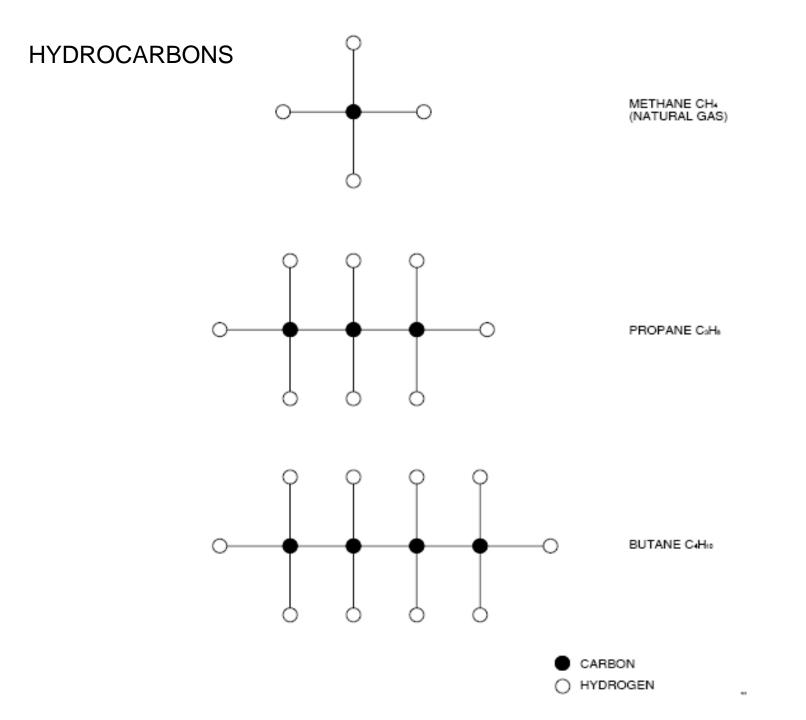
- NG  $\$  SNG  $\$  LPG & the wobbe Index
- Shaving systems & LPG Air mixers
- Cost analysis for several types of fuel (Diesel, LPG, NG & SNG)
- Five \ Designing complete LPG \ SNG \ NG system Case Study & site visit



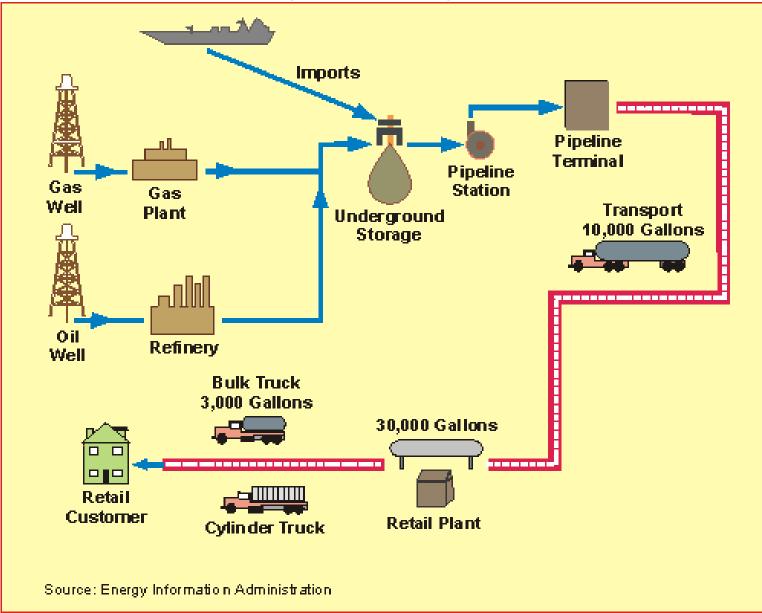


## Part one

# LPG PHYSICAL & Chemical Properties



## Processing & Refining LP-Gases





#### commercial Propane & Butane?

Ideally products referred to as "propane" and "butane" consist very largely of these saturated hydrocarbons; **but during the process** of extraction/production certain allowable unsaturated hydrocarbons like ethylene, propylene, butylenes etc. may be included in the mixture along with pure propane and butane. The presence of these in moderate amounts would not affect LPG in terms of combustion but may affect other properties slightly (such as corrosiveness of gum formation).

Kilojoules = 0.9478 BTU

Kcal = 3.968 BTU

Watt = 3.414 BTU

### APPROXIMATE PROPERTIES OF LP-GASES

Table 1 (Metric)	PROPANE	BUTANE
Formula	C <sub>3</sub> H <sub>8</sub>	C <sub>4</sub> H <sub>10</sub>
Initial Boiling Point, °C	-42	-1
Specific Gravity of Liquid (Water = 1.0) at 15.56°C	0.504	0.582
Weight per Cubic Meter of Liquid at 15.56°C, kg	504	582
Specific Heat of Liquid, Kilojoule/Kilogram at 15.56°C	1.464	1.276
Cubic Meter of Vapor per Liter at 15.56°C	0.271	0.235
Cubic Meter of Vapor per Kilogram at 15.56°C	0.539	0.410
Specific Gravity of Vapor (Air = 1.0) at 15.56°C	1.50	2.01
Ignition Temperature in Air, °C	493-549	482-538
Maximum Flame Temperature in Air, °C	1,980	2,008
Cubic Meters of Air Required to Burn 1 Cubic Meter of Gas	23.86	31.02
Limits of Flammability in Air, % of Vapor in Air-Gas Mix: (a) Lower (b) Upper	2.15 9.60	1.55 8.60
Latent Heat of Vaporization at Boiling Point: (a) Kilojoule per Kilogram (b) Kilojoule per Liter	428 216	388 226
Total Heating Values After Vaporization: (a) Kilojoule per Cubic Meter (b) Kilojoule per Kilogram (c) Kilojoule per Liter	92,430 49,920 25,140	121,280 49,140 28,100
KW / Kg	13.86	13.64



-Similar Properties

-Do not react with each other

-Propane is volatile and boils at -42deg C while Butane is less volatile and boils at 0.6 deg C.

- Both can be stored and transported at moderate pressure.

-Calorific value are almost equal.

-Both are mixed together to attain the vapor pressure that is required.

	TABLE 2 APPROXIMATE VAPOR PRESSURE, PSIG					R		
TU	TURE		PROPANE					TANE
°F	°C	100%	80/20	60/40	50/50	40/60	20/80	100%
-40	-40	3.6	—	—	—	—	—	—
-30	-34.4	8	4.5	_	_	—	—	—
-20	-28.9	1 <b>3</b> .5	9.2	4.9	1.9	—	—	—
-10	-23.3	20	16	9	6	<b>3</b> .5	_	—
0	-17.8	28	22	15	11	7.3	_	—
10	-12.2	37	29	20	17	13	3.4	_
20	-6.7	47	<b>3</b> 6	28	23	18	7.4	—
30	-1.1	58	45	35	29	24	13	$\mathbf{F}$
40	4.4	72	58	44	37	32	18	З
50	10	<b>8</b> 6	69	53	46	40	24	6.9
60	15.6	102	80	65	56	49	30	12
70	21.1	127	95	78	68	59	38	17
80	26.7	140	125	90	80	70	46	23
90	32.2	165	140	112	95	82	56	29
100	37.8	196	168	137	123	100	69	<b>3</b> 6
110	43.3	220	185	165	148	130	80	45



الترفير JD	تكلفة الستهاتك السنوي لنظام JD LPG tanks	تكلفة الاستهلاك السنوي لنظام للاسطوانات JD	الاستهلاك المنوى كغم	الاستهلتك الشهري كغم	الاستهلاك اليومي لتر	عدد الإسطوانات	الاستهلاك اليرمى كغم
734.4	5385.6	6120	18000	1500	89.3	1	50
1468.8	10771.2	12240	36000	3000	178.6	2	100
2203.2	16156.8	18360	54000	4500	267.9	3	150
2937.6	21542.4	24480	72000	6000	357.2	4	200
3672	26928	30600	90000	7500	446.5	5	250
4406.4	32313.6	36720	108000	9000	535.8	6	300
5140.8	37699.2	42840	126000	10500	625.1	7	350
5875.2	43084.8	48960	144000	12000	714.4	8	400
7344	53856	61200	180000	15000	893	10	500



### Odorization :

LP- Gases should be odorized prior to delivery to the bulk plant.

The warding added agent should be detected down to a concentration in air of one-fifth the lower flammability limit LFL or LEL The most common is : Ethyl Mercaptan.

### Combustion:

### **Complete Combustion**

- Water Vapor
- Carbon Dioxide

### **Incomplete Combustion**

- Carbon Monoxide (CO)
- Excessive Water Vapor
- Aldehydes
- Soot

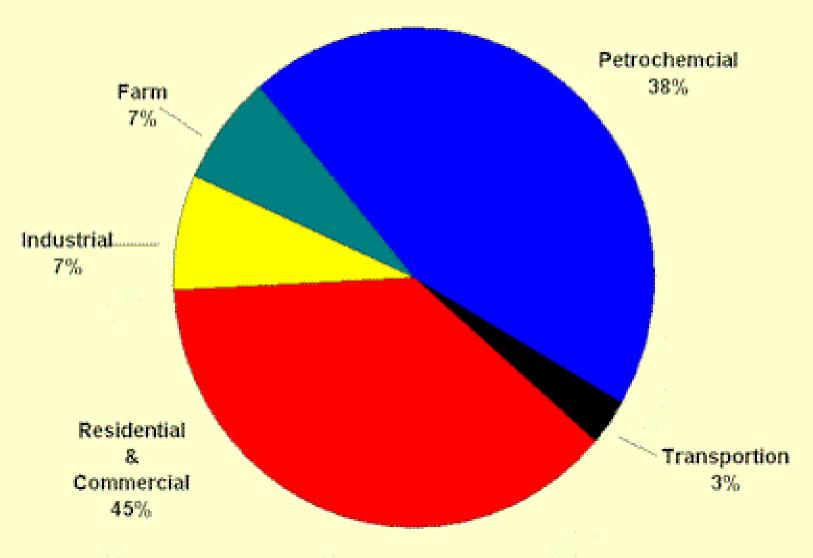
Concentration of CO in Air	Physical Effect
9 ppm (0.0009%)	The Maximum allowable concentration for a short term exposure.
35 ppm (0.0035%)	The Maximum allowable concentration for continuous exposure for in any 8-hour period
200 ppm (0.02%)	Slight headache, tiredness, dizziness, nausea after 2-3H
400 ppm (0.04%)	Frontal Headache within 1-2 Hrs, Life threatening after 3Hrs
800 ppm (0.08 %)	Dizziness, nausea, and convulsions within 45minuts, Unconsciousness within 2 hours, Death within 1 hour
1600 ppm (0.16%)	Headache, dizziness and nausea within 20 minutes, Death within 1Hr
3200ppm (0.32%)	Headache, dizziness and nausea within 5-10 minutes, Death within 30 minutes.
6400 ppm (0.64%)	Headache, dizziness and nausea within 1-2 minutes, Death within 10-15 minutes
12800 ppm (1.28%)	Death within 1-3 minutes

### 10000 ppm = 1% by volume



SOURCE	HEAT POWER	UNIT OF MEASUREMENT	USE OUTPUT	NET CALORIES PER UNIT OF MEASUREMENT	TOTAL CALORIES PER 1000 NET CALORIES	PRODUCT REQUIRED TO BE EQUAL TO 1KG OF PROPANE	UNIT OF MEASUREMENT
Propane	12.000	Cal/Kg	91	10.920	1.099	1	Kg
Natural Gas	9.000	Cal/mc	91	8.190	1.099	1,35	т¢
Aır-Prop.	12.000	Cal/mo	91	10.920	1,099	1	me
Comb. Oil 3-5°E	10.300	Cal/Kg	75	7.725	1.333	1,45	Kg
Diesel	9.000	Cal/I	85	7.650	1.176	1,45	I
Kerasene	8.600	Cal/1	75	6.450	1.333	1,70	I
Wood	3.600	Cal/Kg	40	1.440	2.500	7,5	Kg
Dry wood	5.000	Cal/Kg	45	2 250	2.220	4,8	Kg
Carbon coke	7.000	Cal/Kg	50	3.500	2.000	3,1	Kg
Anthracite	B.000	Cal/Kg	50	4.000	2.000	2,7	Kg
Electricity	850	Cal/Kwh	100	860	1.000	12,7	kW

QUANTITY OF

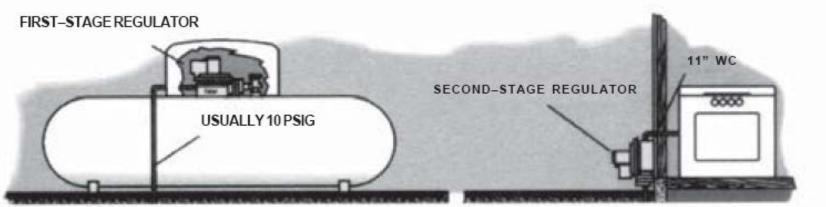


Source: American Petroleum Institute, 2000 Sales of

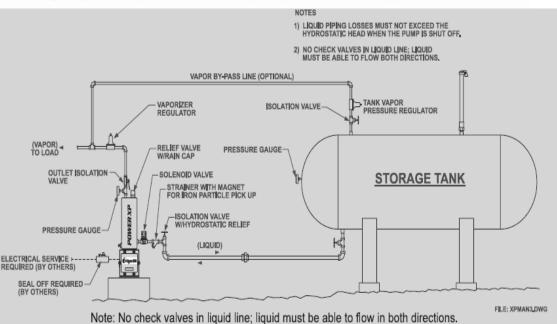


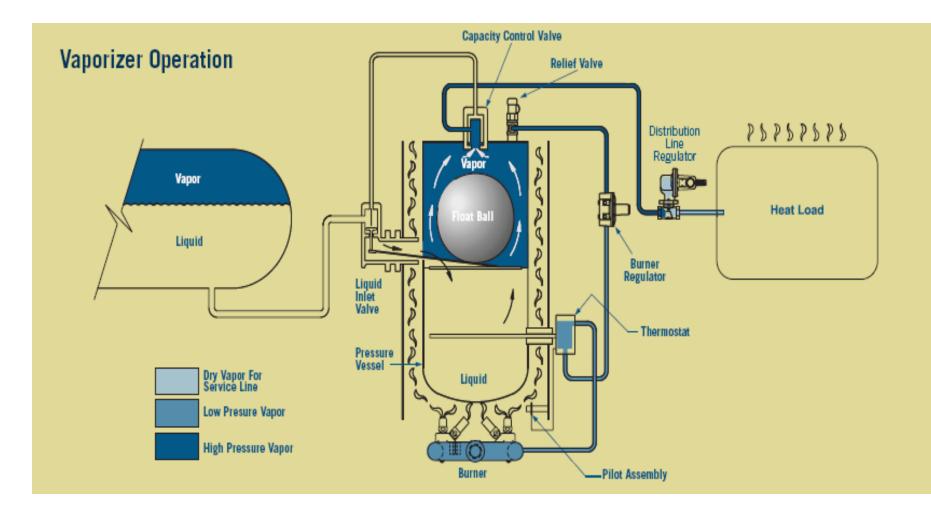
## Part Two

# LPG System Components

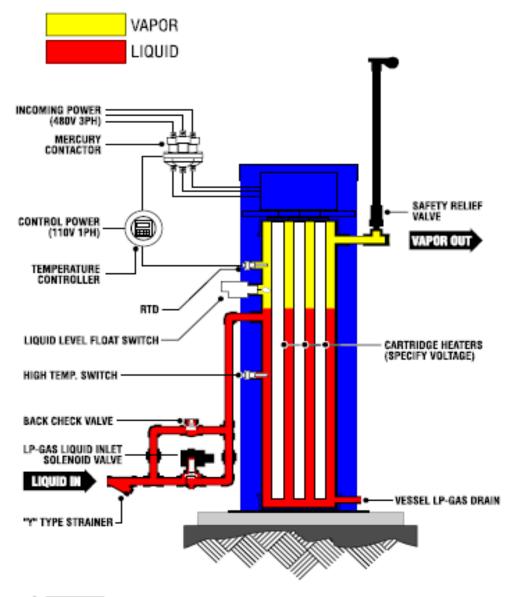


- LPG Tank / Cylinder
- Vaporizer
- 1<sup>st</sup> Stage Regulator
- LPG Feeding Pipe
- 2<sup>nd</sup> Stage Regulator
- Appliance
- Safety Equipment
  - Excess Flow Valves.
  - Relief Valves.
  - Anti- Seismic Valves.
  - Gas Leakage Detectors & Solenoid Valves.





### **RE Series Electric Vaporizer**

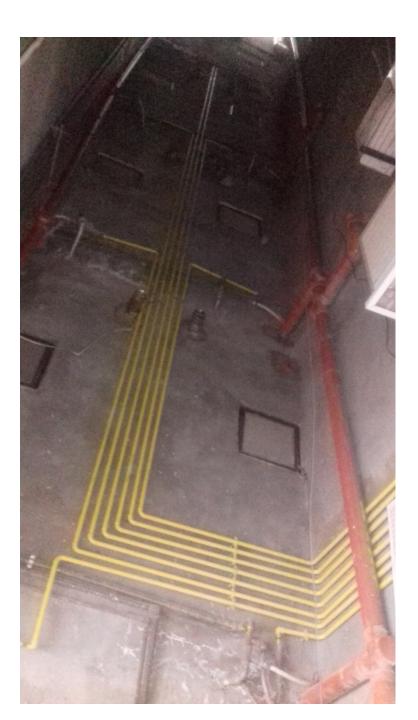












































# LPG Tank - Codes of Design & Manufacturing , ASME versus EN

### PED

European Directive 97/23/EC	Federal Law
Member State Law	State Law
(e.g. UK, Germany, France etc.) Pressure	
Equipment Regulations.	
European harmonised Standards - Norms	Codes recognised by Law
Give presumption of conformity for Essential	e.g. ASME Section I
Safety Requirements (ESR) of PED Annex I	ASME Section VIII/1
(e.g. EN 12952 - Water Tube Boilers	
EN 13445 - Unfired Pressure Vessels)	
Other Standards may be adopted provided that it	
is demonstrated that the PED ESRs are met.	
Notified Bodies or Recognized Third Parties	Manufacturers Approve Welders
Certify Welding Procedures and Welders	
Notified Bodies	Code Inspection Agencies
Performs Design Examinations	Perform Inspections
Performs Inspections for production under the inspection conformity assessment routes.	Endorse Manufacturers Certification
Issues Certificates of Conformity	
Manufactures apply <b>CE</b> Marking and Notified Body unique identification ( <b>Moody International = 1277</b> ) number following issue of Notified Body certification of conformity.	Manufacturer applies Code Stamp
Manufacturer draws up a Declaration of Conformity	Manufacturers Draws up Certification



## PART THREE

## DESIGN ELEMENT OF LP-GAS SYSTEM



Main Design Elements are:

- Total Heat Load Required.
- Determination of Tank Size and quantity required.
- Vaporization capacity of the tanks/cylinders chosen.
- International and Local Standards and Codes obtained.

# **Determining Total Heat Load**

Total Load =  $\Sigma$  appliances heat load in BTU

The best way to determine BTU input is from the appliance nameplate or from the manufacturer's catalog. Add the input of all the appliances for the total load.

Figuring the total load accurately is most important because of the size of the pipe and tubing, the tank (or the number of cylinders), and the regulator will be based on the capacity of the system to be served.

## Table 3 Gas required for common Appliances

TABLE 3 GAS REQUIRED FOR COMMON APPLIANCES					
APPLIANCE	APPROX. INPUT BTU/HR				
Warm Air Furnace Single Family Multifamily, per unit	100,000 60,000				
Hydronic Boiler, Space Heating Single Family Multifamily, per unit	100,000 60,000				
Hydronic Boiler, Space & Water Heating Single Family Multifamily, per unit	120,000 75,000				
Range, Free Standing, Domestic Built-In Oven or Broiler Unit, Domestic Built-In Top Unit, Domestic	65,000 25,000 40,000				
Water Heater, Automatic Storage, 30 to 40 gal. Tank Water Heater, Automatic Storage, 50 gal. Tank Water Heater, Automatic Instantaneous	35,000 50,000				
2 gal. per minute Capacity 4 gal. per minute 6 gal. per minute Water Heater, Domestic, Circulating or Side-Arm	142,800 285,000 428,000 35,000				
Refrigerator Clothes Dryer, Type 1 (Domestic) Gas Fireplace direct vent Gas log	3,000 35,000 40,000 80,000				
Barbecue Gas Light Incinerator, Domestic	40,000 2,500 35,000				

Table Reprinted From Table 5.4.2.1, NFPA 54, 2002 ed.

# Vaporization Rate

Q=kA(Ta-Ts)/Cv

Q [m3)h]; k [kcal/h °C m2]; Ta =ambient Temperature Ts= Temperature correspondent to the vaporization pressure inside the vessel Cv= Latent heat for the liquid to the temperature inside the vessel A= Wet Area

Dependent upon the <u>temperature</u> of the liquid and the amount of "<u>wetted surface" area</u> of the container.

### **Effects**

Withdrawal of gas from one or two containers can lower the container pressure substantially due to the refrigeration of the vaporization gas Regulator capacity is then reduced because of the lower inlet pressure.

### **Solutions**

Multiple cylinders or tanks may be manifolded to give the required vaporization capacity..

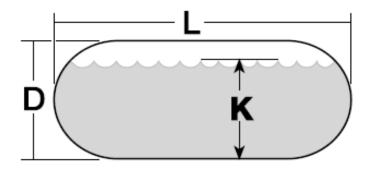
Vaporizers is to be used

## Ruff Estimation of vaporization capacities :

A number of assumptions were made

- 1) The tank is one-half full.
- 2) Relative humidity is 70%.
- 3) The tank is under intermittent loading.

the Table can still serve as a good rule-of-thumb in estimating what a particular tank size will provide under various temperatures.



- D = Outside diameter in inches L = Overall length in inches
- K = Constant for percent volume of liquid in container

UNDER Continuous loading the withdrawal rates in the Table should be multiplied by 0.25

\* Tank frosting acts as an insulator, reducing the vaporization rate.

## Vaporization Rates for 100 Pound DOT Cylinders

Vaporization Rate Table for 100 Lb. DOT Cylinders

TABLE 5 VAPORIZATION RATES IN BTUH FOR VARIOUS TEMPERATURES AND LIQUID LEVELS

#### For continuous draws, where temperatures may reach 0°F, -17 °C, assume the vaporization rate of a 100 lb. cylinder to be approximately 50,000 BTU/HR Therefore : Number of cylinders per side = total load in BTU/HR / 50,000

#### Example:

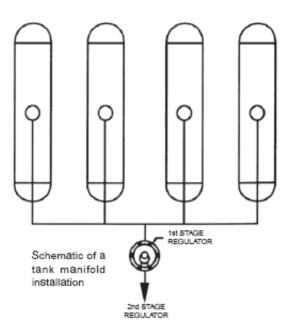
If a total load requirement of 200,000 BTU/HR is to be supplied from 100 pound DOT cylinders and winter temperatures may drop to 0°F, then how many cylinders are needed per side? Number of cylinders per side = 200,000/50,000 = 4

VARIOUS TEIMPERATURES AND LIQUID LEVELS						
LBS. OF PROPANE IN CYL.	-20°F	0°F	20°F	40°F		
100	65,000	71,000	79,000	94,000		
90	60,000	65,000	72,000	85,000		
80	54,000	59,000	66,000	77,000		
70	48,000	52,000	59,000	69,000		
60	43,000	46,000	52,000	61,000		
50	37,000	40,000	45,000	53,000		
40	31,000	34,000	38,000	45,000		
30	26,000	28,000	31,000	37,000		
20	20,000	22,000	25,000	29,000		
10	15,000	16,000	18,000	21,000		

Table 4 Max. Intermittent Withdrawal Rate (BTU/HR)
Without Tank Frosting* if Lowest Outdoor
Temperature (Average For 24 Hours) Reaches

TEMPERATURE	TANK SIZE (GALLONS)			
TEMPERATURE	150	250	500	1,000
40°F	214,900	288,100	478,800	852,800
30°F	187,900	251,800	418,600	745,600
20°F	161,800	216,800	360,400	641,900
10°F	148,000	198,400	329,700	587,200
0°F	134,700	180,600	300,100	534,500
-10°F	132,400	177,400	294,800	525,400
-20°F	108,800	145,800	242,300	431,600
-30°F	107,100	143,500	238,600	425,000

\* Tank frosting acts as an insulator, reducing the vaporization rate.



	PERA-	TABLE 2 APPROXIMATE VAPOR PRESSURE, PSIG						
		PROP	ANE -	$\rightarrow$	► TO		BU	TANE
°F	°C	100%	80/20	60/40	50/50	40/60	20/80	10 <b>0</b> %
-40	-40	3.6	-	_	_	—		—
-30	-34.4	8	4.5	_	-	_	_	—
-20	-28.9	13.5	9.2	4.9	1.9	—	—	—
-10	-23.3	20	16	9	6	3.5	_	—
0	-17.8	28	22	15	11	7.3	_	_
10	-12.2	37	29	20	17	13	3.4	_
20	-6.7	47	36	28	23	18	7.4	—
30	-1.1	58	45	35	29	24	13	
40	4.4	72	58	44	37	32	18	3
50	10	86	69	53	46	40	24	6.9
60	15.6	102	80	65	56	49	30	12
70	21.1	127	95	78	68	59	38	17
80	26.7	140	125	90	80	70	46	23
90	32.2	165	140	112	95	82	56	29
100	37.8	196	168	137	123	100	69	36
110	43.3	220	185	165	148	130	80	45

#### 1 - Standards & Codes

#### NFPA codes & standards used in the LPG Industry

Title	Document No	Application
Cutting , welding & allied processes and cutting & welding process	51 51B	Standards covering the use of fuel gases and fuel / oxygen systems in cutting , brazing and welding
National Fuel Gas Code	# 54	Standards covering Installation of gas piping and appliance in residential and commercial areas
LP-Gas Code	# 58	Standards covering the storage, handling and transportation of LPG
Liquefied Petroleum Gases at utility gas plants	# 59	Standards covering construction and operation of LPG equipment at plants owned by Natural gas utilities.
National Electric Code	# 70	Standards covering the installation of electrical wiring, motors ,electrical controls including hazardous & classified areas
Pleasure & Commercial motor craft	# 302	Standards covering fire protection for boats including LPG systems within
Manufactured Housing	# 501 # 501 A	Standards covering manufactured homes
Recreational Vehicles Recreational Vehicle Parks	# 1192 # 1194	Standards covering installation of gas piping in RV's & Rv's campgrounds
Industrial trucks	# 505	Standards covering type designation, areas of use, maintenance and operation of LPG powered industrial trucks



#### 2- Choosing the Proper Size and Quantity of Tanks

Controlling Elements :

- a) Total Load
- b) Vaporization Rate required.
- c) Location of facility and refilling time interval required.
- d). Physical Place Available.

## Container Locations & preparations 1- General Conditions / NFPA 58

Located outside of buildings	6.2.1
Separation Distances between containers, Important buildings and other properties / Table 6.3.1* Distance is measured from the relieve valve / filling connection	6.3.1
Distance from point of discharge of the relief valve of a container or	6.3.9
vents or container filling connection, to any openings, or source of ignition to be as table 6.3.9	6.3.10
The horizontal distance between any portion of the building that overhangs out of the building wall (balcony) and the underneath Gas Tank bigger than 473Liter shall be 50% of the distances given in table 6.3.1 conditioned that it is less than 15m above the tank and extend more than 1.5m from the building	6.3.12
No loose or piled combustible material and weeds and long dry grass within 3m distance.	6.4.5.2
LPG containers to have minimum 3m separation distance from wall of diked areas containing flammable or combustible liquids	6.4.5.4

Separation between LPG tanks and tanks containing flammable or combustible liquids if either is above ground while the other is underground.	6.4.5.6
No structures around the LPG tanks other than a fence for security against tampering	6.4.7
Point of transfer of containers located in stationary installations if it is NOT located at the container, it shall be located in accordance with table 6.5.3	6.5.3
Protection from damage from vehicles.	6.6.1.2
All operating appurtenances of the container are accessible	6.6.1.5
Where high flood waters that may result of tank floatation is possible , tanks to be securely anchored.	6.6.1.6

## **Container Locations & preparations**

#### 2- Above Ground Tanks

Single installation of Above Ground Containers > 0.5m <sup>3</sup> but less than 4.5 m <sup>3</sup> have a reduced distance of 3 meter from an important building	6.2.1
For Buildings devoted to gas distribution/ manufacturing and made of other than wood-frame, distance shall be reduced to 3 meters regardless size of tank.	6.3.1
For multi-container installation less than 500 Liters that are manifolded	6.3.9
together ; exceeding 1900 Liters hall be considered with the aggregated water capacity for the distances from important building . No separation among the aggregated tanks is required.	6.3.10
Above ground multi-container installation composed of several 45m <sup>3</sup> or more shall have limited No. of tanks per group with separation distances between groups a per table 6.4.2 unless provisions 6.24.3 and 6.24.4 are met then distance is reduced to 50% of that mentioned in table 6.4.2	6.3.12
Minimum horizontal distance separate above ground LPG tanks from above ground flammable tank storage material with flash point of les than 93.4°C other than LPG hall be 6m.	6.4.5.2
Any Part of Above Ground LPG tank shall not be located within 1.8m of a vertical plane beneath overhead electrical power line <b>over 600 V</b> .	6.4.5.4

Horizontal Containers Structural Support	6.6.3.1
Interconnected Tanks to have same level of elevation	6.6.3.2
Horizontal permanent containers attached with the same support must comply to table 6.6.3.3.	6.6.3.3
The part of he container in contact with the foundation shall be coated or protected to minimize corrosion.	6.6.3.5
Where snow accumulation anticipated is more than the height of the container, excluding the dome, then a take or other marking to be present and container to be fixed preventing it movement resulting from snow accumulation.	6.6.3.6

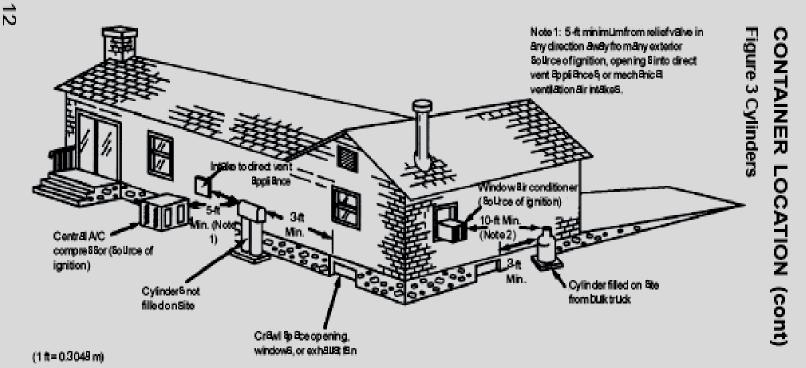
# Container Locations & preparations 3- Underground

Containers of <b>7.6m3</b> to <b>114 m3</b> water capacity satisfies all provisions of section 6.24 shall have a reduced distance of 3 meters only from important buildings.	6.3.4
No part of the underground tank is less than 3 meters from a building or line of adjoining property that can be built upon (another future building if to be existed within the adjoining property)	6.3.4.2
For Mounded containers, No part that I installed above grade shall be less than 1.5 meter from a building.	6.3.4.3
Containers to be located outside of any building	6.4.4.1
Buildings shall not be constructed over any underground or mounded container.	6.4.4.2
The sides of adjacent containers shall be separated in accordance with Table 6.3.1 but not les than 1 meter	6.4.4.3
No limited number of containers for one group if it is installed parallel with ends in line.	6.4.4.4

Where more than one raw of containers is installed the adjacent ends of the containers in each row shall be separated by not less than 3 meters.	6.4.4.5
<ul> <li>Installation of underground containers in accordance with the following;</li> <li>In areas with no vehicle traffic; minimum 15 cm below grade.</li> <li>In areas where traffic is expected; either a minimum of 46cm below grade or protection from damage from vehicles.</li> <li>Protection shall include fitting and tank connections against vehicular damage.</li> <li>Protection to be done if traffic is expected within 3 meters from the container.</li> <li>Vents and relief pipes to be above highest probable water level.</li> <li>Container is set leveled and surrounded by earth or sand firmly tamped in place.</li> </ul>	6.6.6.2
Mounded containers to be mounded by earth or sand or other non combustible material and covered of at least 30 cm.	6.6.6.3.(1)

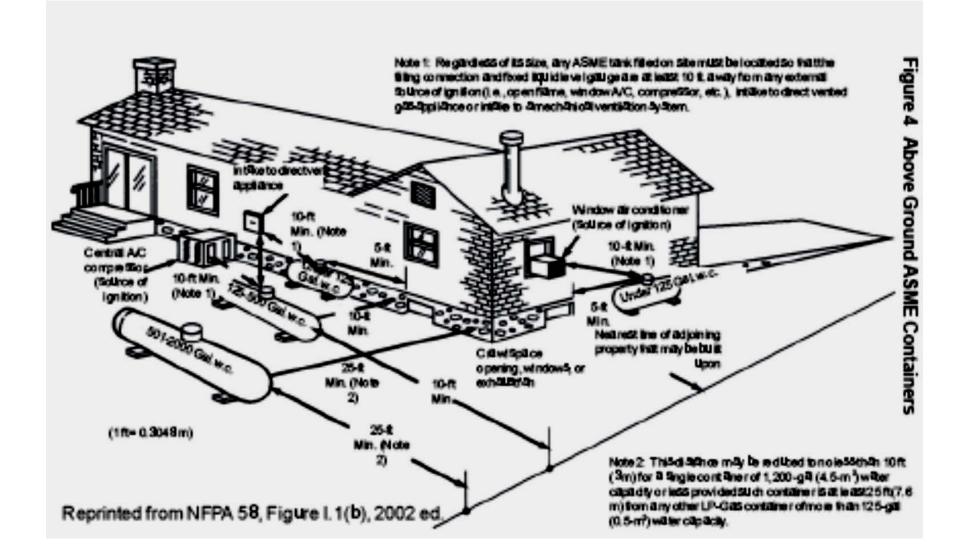
Container valves and appurtenances to be accessible.	6.4.4.5
If mounded container bottom is 76cm or more above the surrounding	
grade; access to bottom connections if any to be provided and this	
connection to be considered as part of the container with all code	
applies on it.	

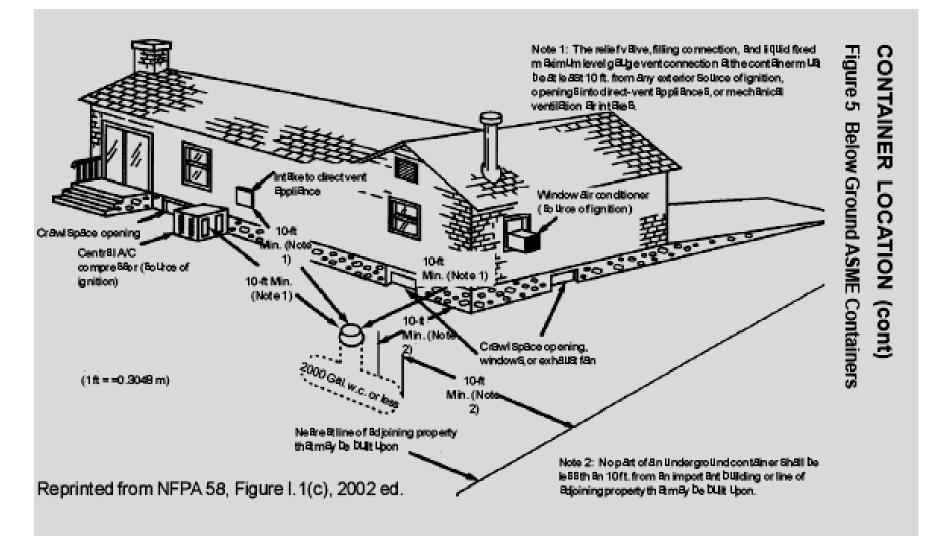
\*\*Distance for all underground and mounded containers shall be measured from the pressure relief valve and filling connection. (Article 6.3.4.1 // Page 58-27).



Note 2: If the cylindler is filled on Ste from & bulk trück, the filling connection and vent valve multi be at least 10-ft from any exterior Solice of ignition, opening 8 into dire d-vent appliances, or mechanical ventilation air intakes.

Reprinted from NFPA 58 Figure I.1(a), 2002 ed.





# **Tank Preparation**

#### **REMOVING WATER FROM CONTAINERS**

Water in LP-Gas cylinders and tanks can contaminate the gas, causing regulator freezeups and erratic appliance performance.

Adding anhydrous methanol (99.85% pure) will neutralize any moisture within the container.

This will minimize freeze-up problems for normal amounts

of water in a container.

Table 6		
CONTAINER SIZE	MINIMUM AMOUNT OF METHANOL REQUIRED	
100 lb. cylinder	1/8 Pint (2 fluid ounces)	
150 gal. tank	1 pint	
250 gal. tank	1 quart	
500 gal. tank	2 quarts	
1000 gal. tank	1 gallon	

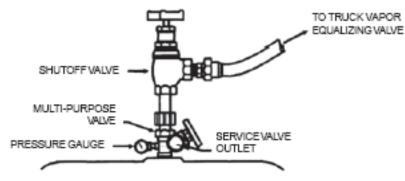
Warning: Do not substitute other alcohols in place of methanol.

## **PURGING AIR FROM CONTAINERS**

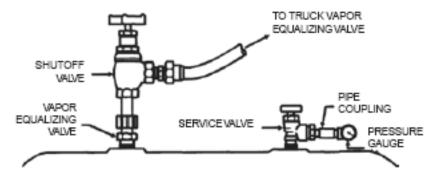
Air in the LP-Gas can cause appliance pilot lights to be extinguished easily. It can also lead to excessive container pressure, making the safety relief valve open.

- 1) Bleed the air to atmosphere by opening the multi-purpose valve or the service valve for several minutes until air pressure is exhausted. Close the valve.
- 2) Attach the truck vapor equalizing hose to the multipurpose valve's vapor equalizing valve or the separate vapor-equalizing valve.
- 4) Slowly open the shutoff valve on the end of the hose so that the truck excess flow check valve does not slam shut.
- 5) Closely watch the pressure, and when the gauge reaches 15 psig, close the shutoff valve.
- 6) Open the vapor service valve on the multi-purpose valve or the separate service valve, Allow all pressure to be exhausted before closing the multi-purpose valve or the service valve.
- 7) Repeat steps 4 through 6 at least **three** more times to make certain air has been purged from the tank.

#### PURGING METHOD WITH MULTI-PURPOSE VALVE



#### PURGING METHOD WITH SEPARATE VALVES



Note: Do not purge tanks in this way on the customer's property. Purge them in a safe place at the bulk plant site.

## **Pipe Selection**

- Essential for efficient operation.
- Deigned for Maximum gas demand + Future expansion.

Factors affects the selection of type of pipe to be used:

- Location ; indoor or out door.
- State of Gas : Liquid or Vapor.
- Pressure .
- Risk of mechanical damages.

Type of Pipe :-

- Wrought iron/ Steel Pipe; Installed as per ASME B31.3, welded as per ASME V111,
- Copper ; Seamless tube/ pipe, Type K or L
- PE; high density pipe. (out door + under ground + Pressure< 30 psig)

Four different areas of sizing requirements must be addressed:

- 1) Sizing between First-Stage and Second-Stage Regulators
- 2) Sizing between Second-Stage Regulator and Appliance
- 3) Sizing between 2 PSI Service and Line Pressure Regulators
- 4) Sizing between Line Pressure Regulator and Appliance

Service	Schedule 40	Schedule 80
Liquid	Welded	Threaded or Welded
Vapor ≤125 psig	Threaded or Welded	Threaded or Welded
Vapor > 125 psig	Welded	Threaded or Welded

### Directions for Sizing between First-Stage and Second-Stage Regulators (Based on NFPA 54 Hybrid Pressure Method)

1) Measure the required length of pipe or tubing from the outlet of the firststage regulator to the inlet of the second-stage regulator.

 Determine the maximum gas demand requirements of the system by adding the BTU/HR inputs from the nameplates of all the appliances or by referring to Table 3 on page 5.

3) Select the pipe or tubing required from Tables 7a, b,and c on pages 23-25.

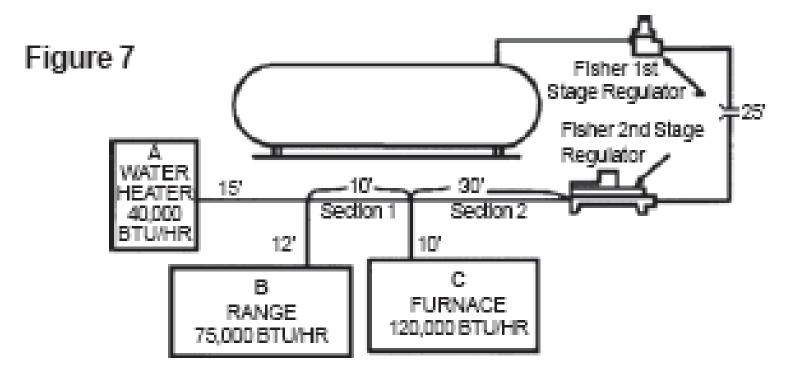
# Directions for Sizing Between Second-Stage Regulator and Appliance (Based on NFPA 54 Longest Length Method)

- Measure the length of pipe or tubing from the outlet of the secondstage regulator to the most remote appliance.
   (Note: This is the only length needed to size the second-stage system.)
- For each outlet and section of pipe, determine the specific gas demand requirements by adding the BTU/ HR inputs from the nameplates of each appliance or by referring to Table 3 on page 5.
- 3) Select the pipe or tubing required for each section from Table 8a or 8b on pages 26 and 27.

Determine the sizes of pipe or tubing required for this two-stage LP-Gas installation.

#### Example:

A private home is to be supplied with a LP-Gas system serving a central furnace, range and water heater. The gas demand and piping lengths are shown on the sketch below.



#### For First-Stage:

1) Length of first-stage piping = 25 feet (round up to 30 ft. for use in Table 7a, b, c.).

2) Total gas demand = 40,000 + 75,000 + 120,000 = 235,000 BTU/HR.

 From Tables 7a, b, and c, use 1/2" iron pipe; or 1/4" Type L or <sup>3</sup>/<sub>4</sub>" CR copper tubing or 1/2" plastic tubing. (Assume a 10 psig first-stage regulator setting and a 1 psig pressure drop.)

#### For Second-Stage:

- 1) Total second-stage piping length = 30 + 10 + 15 = 55 feet (round up to 60 ft. for use in Table 8a and 8b).
- 2) Gas demand requirements and pipe selection from Table 8a and 8b (Assume a 11" w.c. setting and 1/2" w.c. pressure drop):

For Outlet A, demand = 40,000 BUT/HR, use 1/2" iron pipe or 3/8" Type L or 5/8" ACR copper tubing.

For Outlet B, demand = 75,000 BUT/HR, use 1/2" iron pipe or 1/2" Type L or 5/8" ACR copper tubing.

For Outlet C, demand = 120,000 BUT/HR, use 3/4" iron pipe or 5/8" Type L or 3/4" ACR copper tubing.

For Section 1, demand = 40,000 + 75,000 = 115,000 BTU/HR, use 3/4" iron pipe or 5/8" Type L or 3/4" ACR copper tubing.

For Section 2, demand = 40,000 + 75,000 + 120,000 = 235,000 BTU/HR, use 1" iron pipe.



## **Pipe Selection Tables**

#### RESISTANCE OF VALVES & FITTINGS IN EQUIVALENT FEET OF PIPE

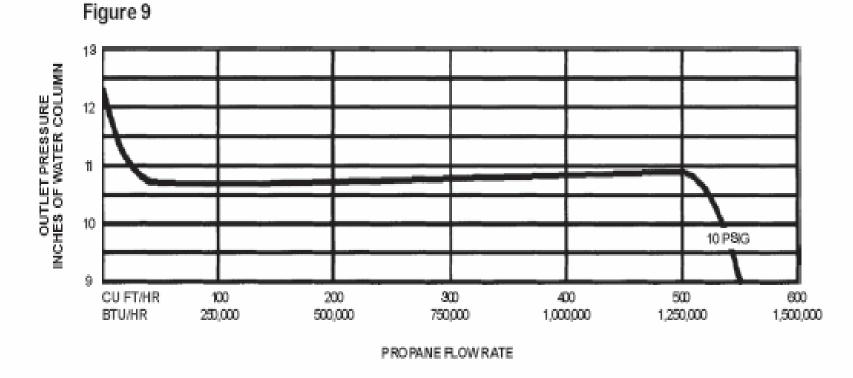
	PIPE SIZE						
	1	1 1⁄4	1 ½	2	2 1/2	3	4
Elbow 90	4	4 1/2	5	6	8	9	11
Elbow 45	1	2	2	2 1/2	3	4	5
Tee thru side	6	8	9	12	14	17	22
Y strainer same size as pipe	25	25	25	42	42	42	60
Y strainer next larger size	16	16	16	16	14	20	
Globe valve	28	35	45	60	65	85	120
Angle valve	15	19	22	28	35	42	57
Ball valve	1/2	1/2	1/2	1/2	1/2	1/2	1/2
Quick-closing gate	3	3	3	3	3	3	3

Above values are approximate and will vary from one manufacturer to another

#### SELECTING THE REGULATOR

#### **Effective elements:**

- 1 Total Load Requirement.
- 2 Inlet Pressure
- 3 Outlet Pressure
- 4 Regulator performance curves
- 5 Type of Gas used
- 6- Pipe Size



The figure above shows a performance curve which demonstrating the capacity of a regulator at different inlet pressures, given the factory setting for outlet pressure.

#### **TWO-STAGE REGULATION**

#### Advantages of Two-Stage Regulation

**Uniform Appliance Pressure** - Two-staging lets the first stage regulator supply a nearly constant inlet pressure to the second-stage regulator at the house. This means the second-stage regulator has an easier time of maintaining appliance pressure at 11" w.c., thus improving the system efficiency.

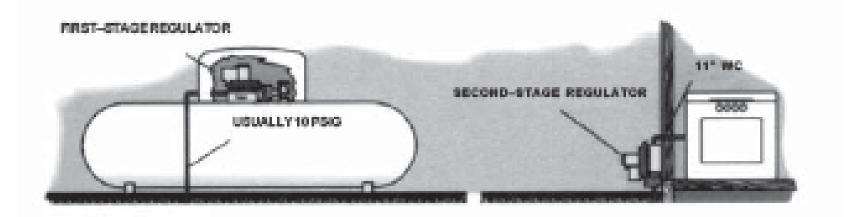
**Lower Installation Costs** - Smaller pipe or tubing can be used between the first and second-stage regulators due to the higher pressure, thus reducing installation and piping material costs.

**Freezeups** - Two-stage systems reduce problems due to regulator freezeups caused by excessive water in gas. Larger orifices make it more difficult for ice to form and block the passage area. The expansion of gas at two different orifices in a two-stage system greatly reduces the "refrigeration effect" that causes freezeups.

**Flexibility of Installation** - A high pressure regulator can feed a number of low pressure regulators, thus enabling the addition of appliances in the future to the same pressure line without affecting their individual performance.

**Fewer Trouble Calls** - With two-stage regulation, you can expect fewer trouble calls due to pilot outage or burner adjustment. This means higher appliance efficiency, lower service costs and better customer relations.

#### **REGULATOR INSTALLATION**



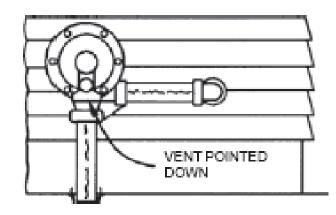
#### TWO-STAGE REGULATION

#### Two Regulators, one at tank and one at building, reduce pressure down to burner pressure (11" w.c.)

#### **Regulator Vents**

#### **Outdoor Installations**

A regulator installed outdoors without a protective hood must have its vent pointed vertically down, as shown in the drawing.



-The regulator should be at least 18 inches above ground.

-Do not install the regulator where there can be excessive water accumulation or ice formation, such as directly beneath a downspout, gutter or roofline.

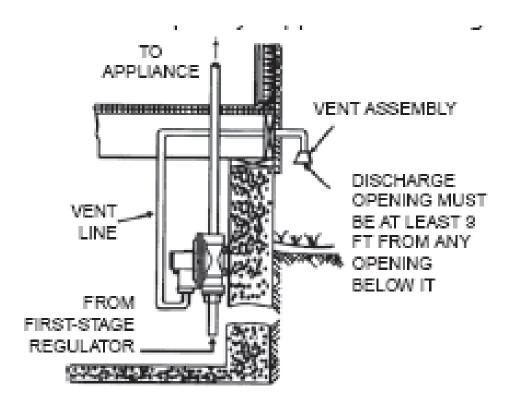
- All vent openings must be at least three horizontal feet from any building opening and no less than five feet in any direction from any source of ignition, openings into direct vent appliances or mechanical ventilation intakes.

- Horizontally mounted regulators, such as on single cylinder installations, must be installed underneath a protective cover. On ASME tank installations with the regulator installed under the tank dome, the regulator vent should slope slightly down enough to allow any condensation to drain from the spring case. The regulator vent should be positioned far enough back from the tank dome slot so that it is protected from the weather. The hood should be kept closed.

#### Indoor Installations

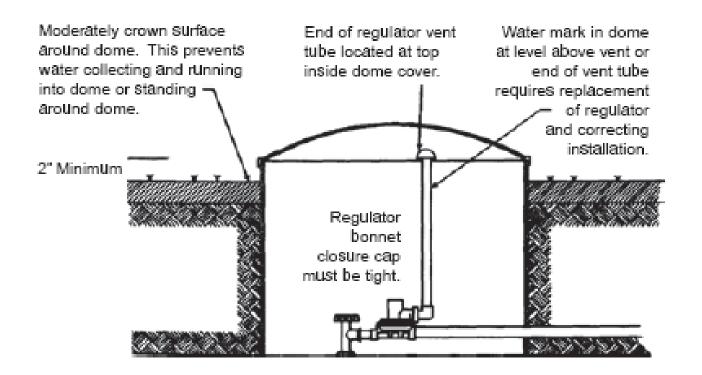
In a fixed pipe system, regulators installed indoors require a vent line to the outside air.

A screened vent assembly must be used at the end of the vent line. The vent assembly position and location precautions are the same as for regulator vents. The vent line must be the same size as the regulator vent and adequately supported. See Figure below.



#### Underground Tanks

A vent tube is required on these installations to prevent water from entering the regulator's spring case. The vent tube connects to the regulator vent and terminates above any possible water level, see Figure below. Be sure that the ground slopes away from the tank dome as illustrated. See Figure below.





# Part Four

Natural Gas Vs LP-Gas

		NG	Propane	Butane	
Chemical formula		CH4	C3H8	C4H10	
Boiling point of liquid at atmospheric press	sure	(- 162 °C	-42 °C	0°C	
Specific Gravity of vapor (Air = 1)		0.6	1.53	2.0	
Specific Gravity of liquid (Water = 1)		0.6	0.51	0.58	
Calorific value @ 60 °F (15°C)	BTU/CFT BTU/ m <sup>3</sup> Kcal / m <sup>3</sup>	1012 35901 9047	2516 88906 22,404	115901 11	127 0495 7845
Latent heat of vaporization	Kcal/Kg		785	808	
Liquid weight	Kg / Liter		0.508	0.576	
Vapor volume from 1 liter of liquid at 15 °C	; m <sup>3</sup>		0.272	0.234	
Vapor volume from 1 kg of liquid at 15 °C	M <sup>3</sup>		0.534	0.406	1
Combustible limits % of gas in Air		5 - 15	2.4 - 9.6	1.9 - 8.6	1
Amount of air required to burn 1 m3 of gas	s m <sup>3</sup>	9.53	23.86	31.02	
Ignition temperature in air	°C	650	490 - 550	480 - 540	1
Maximum flame temperature in air	°C 🤇	1964	1980	1991	Þ
Octane Number		100	Over 100	92	

All data is approximate. For actual properties of any particular batch, contact your fuel supplier.

		NG	Propane	Butane
Chemical formula		CH4	C3H8	C4H10
Boiling point of liquid at atmospheric pressure		- 162 °C	-42 °C	0 °C
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Specific Gravity of liquid (Water = 1)		0.6	0.51	0.58
Calorific value @ 60 °F (15°C)	BTU/CFT Kcal / m³	1012 9005	2516 22,390	3280 29,190
Latent heat of vaporization	Kcal/Kg		785	808
Liquid weight	Kg / Liter		0.508	0.576
Vapor volume from 1 liter of liquid at 15 °C	C m <sup>3</sup>		0.272	0.234
Vapor volume from 1 kg of liquid at 15 °C	m³		0.534	0.406
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All data is approximate. For actual properties of any particular batch, contact your fuel supplier.

Several characteristics affect Liquified Petroleum Gas (LPG) as a replacement fuel.

These include :

- 1 Flame Velocity and Color
- 2 Specific Gravity
- 3 Calorific Value
- 4 BTU Measurement (Wobbe Index )

#### 1 - Flame Velocity and Color

Because of the different number of carbon atoms in propane, propane-air mixtures produce a flame that is more yellow in color than that of natural gas. However, the yellow tips are not of any consequence and do not affect burner operation or efficiency. Flame velocities of LPG are near equal to that of natural gas. Therefore, there is no significant flame lift difference between natural gas and propane-air mixtures.

#### 2 - Specific Gravity

The density of gas, relative to air, is called specific gravity. The specific gravity of air is defined as 1. Since propane gas has a specific gravity of 1.5, propane-air mixtures have a specific gravity of greater than 1.

3 - The Wobbe Index, a critical factor when analyzing LPG-Air plant requirements, is a function of gas quality and allows matching one gas (in this case, natural gas) to a replacement gas (in this case, LPG-Air). If the two different gases have an identical Wobbe Index, they will produce an equal amount of heat and combustion products and will require the same amount of combustion air. Burners, adjusted for a specific calorific value and fitted with a replacement orifice to match a lower Wobbe Index, result in minor combustion changes. Substituting a gas for one with a higher Wobbe Index, generally allows a narrow acceptance range. Flame characteristics determine the acceptance range for the replacement gas.

# Wobbe Index

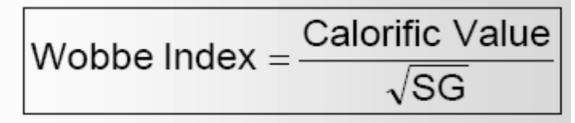
Goffredo Wobbe , Physicist , Bologna, Italy, 1927

- The heat output of a burner at constant gas pressure at constant orifice size is proportional to the flow volume per time. (The longer you run the burner, the more heat is being put out.)
- The flow velocity through a given orifice size at constant pressure is proportional to the specific gravity (SG) of a gas. (The lighter a gas molecule is, the more molecules can pass through a fixed-size orifice.)
- 3. The calorific value (CV) of a gas is proportional to its specific gravity (SG). NG 1000 BTU/ft3 SG=0.61 à 1640 C3 2516 BTU/ft3 SG=1.53 à 1644 C4 3280 BTU/ft3 SG=2.00 à 1640

Combining the three ideas, we can come up with a formula that allows us to compare the flow characteristics of two gasses.

If we know their CVs or SGs, we can determine whether they produce similar heat outputs when used with the same orifice.

Mr. Wobbe's Formula



He decided to keep the number dimension -less to avoid confusion with CV.

#### Wobbe Index

Wobbe Index Explanation (from American Gas Association Bulletin No. 36)

The Wobbe number, or Wobbe index, of a fuel gas is found by dividing the high heating value of the gas in Btu per standard cubic foot by the square root of its specific gravity with respect to air. The higher a gases' Wobbe number, the greater the heating value of the quantity of gas that will flow though a hole of a given size in a given amount of time. It is customary to give a Wobbe number without units—even though it has the dimensions Btu per scf—because to do so would lead to confusion with the volumetric heating value of the gas.

In almost all gas appliances, the flow of gas is regulated by making it pass through a hole or orifice. The usefulness of the Wobbe number is that for any given orifice, all gas mixtures that have the same Wobbe number will deliver the same amount of heat. Pure methane has a Wobbe number of 1363; natural gas as piped to homes in the United States typically has a Wobbe number between 1310 and 1390.



Wobbe Index = 
$$\frac{\text{Calorific Value}}{\sqrt{SG}}$$
  
Wobbe Index = 
$$\frac{1000 [BTU / cuft]}{\sqrt{0.61}} = \frac{1000}{0.781}$$

Wobbe Index of Natural Gas = 1280

## Wobbe Index of Natural Gas

SG	0.59	0.6	0.61	0.62									
Sqrt(SG)	0.7681	0.7746	0.7810	0.7874									
CV	Wobbe Index												
950	1237	1226	1216	1207									
980	1276	1265	1255	1245									
1000	1302	1291	1280	1270									
1050	1367	1356	1344	1334									

# Wobbe Index of LPG/Air Mix

- $SG_{SNG} = 1.28 \text{ to } 1.32$
- $\sqrt{1.28} = 1.1313$
- $\sqrt{1.32} = 1.1489$
- $CV_{SNG} = 1292 BTU/cuft @ 1.28$ 
  - to 1476 BTU/cuft @ 1.32
- Wobbe<sub>SNG</sub> = 1142 @ 1.28 to 1284 @ 1.32

#### **Typical Mixed Gas Settings**

SG (SNG) = 1.28 to 1.32

, Specific Gravity

CV (SNG) = 1292 BTU/cuft @ 1.28

, Calorific Value

to 1476 BTU/cuft @ 1.32

Ratio <sub>(SNG)</sub> = 51/49 Vapor/Air @ 1.28 to 58/42 Vapor/Air @ 1.32

SNG = Synthetic Natural Gas

# Consider the Wobbe Index !

- Wobbe<sub>SNG</sub> ||42 @ |.28 = 1284 @ 1.32 to
- 1000 BTU/cuft =
- CV<sub>NG</sub> SG<sub>NG</sub> 0.61 =
- Wobbe<sub>NG</sub> =
- 1280

Wobbe Index changes :

Natural Gas changes due to : Seasonal Changes or the Source may change

LPG Mixture due to : Propane / Butane Composition

# How much Wobbe Change is Acceptable

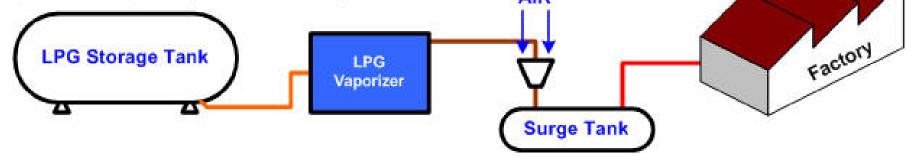
- Less than 5% deviation is desired
- Depending on how much SNG you have in your PANG\*, the WobbeSNG should be maintained at better than +/- 10%

\*PANG = Propane Air Natural Gas

Typical max. LP/Air is 50% of total to maintain the SGPANG lighter than Air.

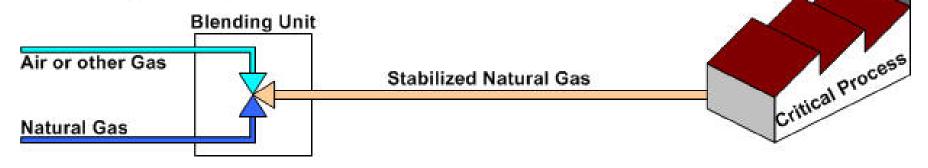
#### Create LP/Air Mixture (Synthetic Natural Gas) to replace Natural Gas

If the supply of Natural Gas is interrupted, these systems produce a mixture of LP Vapor and Air with properties that are equivalent to those of Natural Gas. This allows users to continue using their Natural Gas equipment without having to switch to equipment that can handle other fuel sources (like fuel oil, coal, etc.). Commercial and industrial users can take advantage of steep discount on Natural Gas, offered by their gas utility company, if they agree to be curtailed when demand on Natural Gas exceeds supply. These discounts are usually sufficient to amortize the purchase price of a complete system in under 2 years.

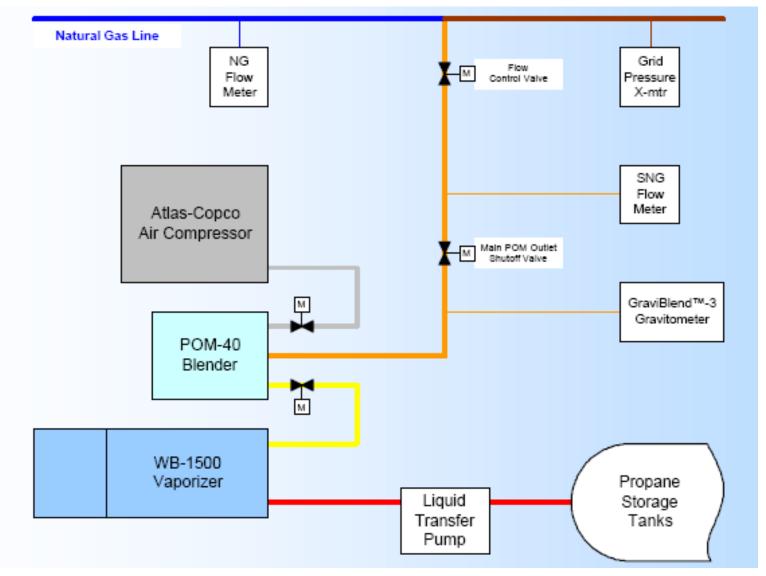


#### Conditioning of Natural Gas to obtain consistent Calorific Values

In certain critical manufacturing processes, even small fluctuations in the Calorific Value of Natural Gas can create wide swings of burner output temperatures, resulting in product quality problems, or even complete loss of the manufacturing batch. AES Gas Blending Systems take the Natural Gas as supplied by the utility company and blend it with Air, Nitrogen, LP, or another conditioning gas. The blending ratio is variable, and is automatically controlled through sensors in the output stream of the system, measuring the actual gas properties. The result is Natural Gas with consistent, pre-defined and very well repeatable heating values. Examples of processes that can benefit from this technology include glass kilns, ceramic kilns, heat treatment plants, etc.

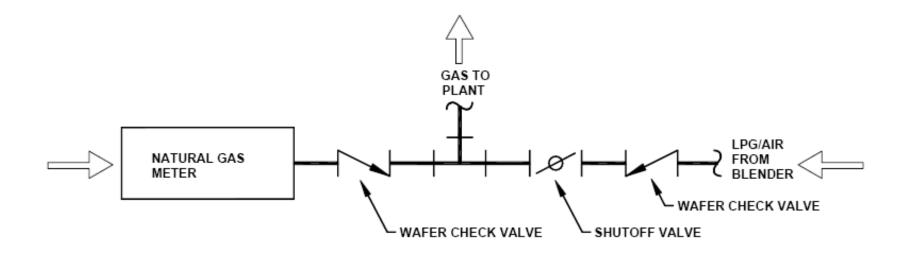


# PeakShaving System Components





# Natural Gas to SNG Tie-In Detail



TYPICAL TIE-IN DETAIL



#### LPG AS VEHICLE FUEL

#### ADVANTAGES OVER CNG

- LPG kit is 30 40 % cheaper than CNG.
- No significant power loss as in CNG.
- LPG tank is very light as compared to CNG.
- Filling time of LPG is up to 40 liters / minute , CNG takes a long time to fill.
- LPG can easily be available in almost every patrol station
- Distance covered after filling tank once is almost double in LPG than CNG.



## Part 5

# Case Study // Design of a complete LPG system with LPG / SNG / NG distribution Network

	Point CONSUMPTION / PRESSURE DROP Point Point Point						Doint	CC			PRESSURE I			Delint	CC				SSURE DROP			
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		WDTO	M3/H PD	M3/H	PD N	M3/H	PD		NID I U	M3/H	PD	M3/H PD	M3/H	PD		WDTO	M3/H	PD M3	/H PD	M3/H	PD	
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<b>\$</b>	At 15	dea C.	, 1kg/h L	PG = 0.	436 c	ubic	meter /ł	h			~	UBTU		IRTU			mb	$\lesssim$	12			
$\left( \right)$		-									(14)3	W		3 M					<u> </u>			
а Э			ne MBTU/ł			,				3 mtr	<u> </u>					40			$\odot$			
ne _	For N	atural	Gas ; eacł	n one M	BTU =	=/~ '	28.3 M3	/h		, s. h	<sup>ko</sup>				12	s. /						
()	For S		e MBTU/h	- / ~ /	0 M3	/h			5	φ <sup>.</sup> "		* MBTU	< 10		Ψ_	15 mtr						
NETU	101 31	10, 01		- /.5 .	LU IVIU	/ 11					ρ _(	UTU	- DE	mtr		-						
3 "									3		( <sup>5</sup> )5	WP.	. ME	$\geq$								
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$\mathbb{Q}$																						
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